

Challenges in the observation of radiation fluxes over land and ocean

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Rational: Land and Ocean communities to interact in the frame of radiation measurements

- Immediate goal: Establish a dialog across communities to harmonize the different methods of in-situ and remote sensing assessment of surface radiation balance
- Long-term goal: Establish the foundation for integrating surface shortwave and longwave radiation measurements into global fields.
- Share knowledge and experience across different comms
- Document calibration methods
- Assess uncertainties of different methods
- Improve in-situ sampling
- Validate and assess climate models / satellite products
- Contribute to understanding of earth's energy balance
- www.oceandecade.org, airseaobs.org, www.oceanbestpractices.org, ...

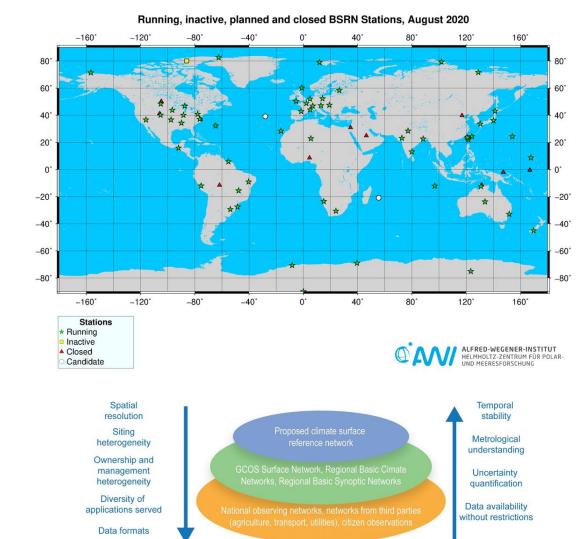






Land / BSRN approach

- Stations Representative of wider areas. Acting as radiation reference network over Land for climate monitoring, climate model and remote sensing products validation
- Established in early 90's with ~20 stations
- Host data from 70+ stations across the world (land) different surface type and climate regimes over ~30 years
- Candidate (8+2)/ Operational (57) / Inactive (0)
 / Closed (16) (Update: Apr 2021)
- Geographical gaps still an issue on some areas
- Archive (AWI) <u>www.pangaea.de</u> (11,000+ monthly)



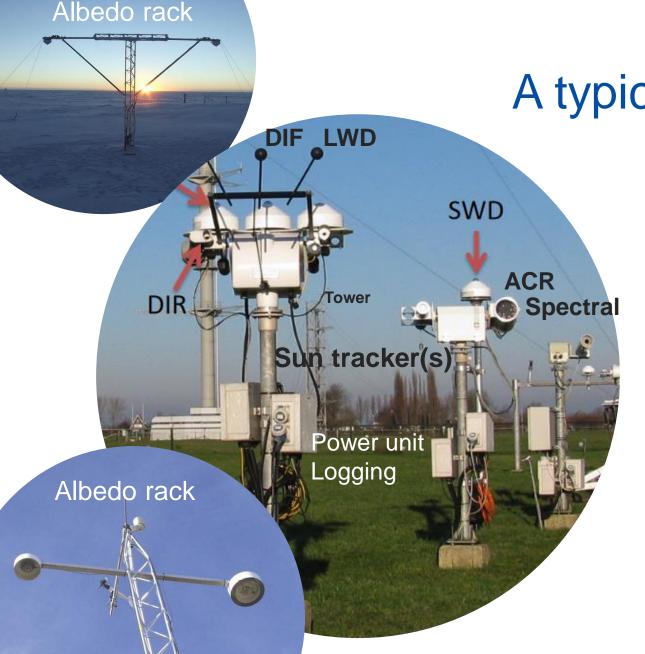
(P.Thorne et al., IJC JC2018)











A typical BSRN station collects

- Basic measurements
 - the downwelling components of the **shortwave** (glo, dif, dir) and **longwave** (lwd) broadband radiation at the surface



- Temperature, pressure, RH (2m)
- Extended measurements:
 - reflected shortwave (swu) and longwave (lwu) to close the radiative budget at the surface



- 3m, 10m, 30m
- Upper air, UVa UVb, spectral, ...



Equipment of a BSRN station

- Thermopiles
 - Pyranometer (swd, swu and dif)
 - Pyrheliometer (dir normal)
 - Pyrgeometer (lwd, lwu)
- Sun tracker/albedo rack
- Datalogger









Table 1 - Pyranometer classification list

Specifica- tion param- eter No. (see <u>4.3.2</u>)	Parameter	Name of the classes, acceptance intervals and widt of the guard bands (in brackets)		
	Name of the class	A	В	С
	Roughly corresponding class from ISO 9060:1990 ²)	Secondary standard	First class	Second class
a	Response time (see also 4.3.3 on fast response pyranometers):	< 10 s (1 s)	< 20 s (1 s)	< 30 s (1 s)
	time for 95 % response			
b	Zero off-set:			
	a) response to -200 W·m ⁻² ne thermal radiation	±7 W·m ⁻² (2 Wm ⁻²)	±15 W·m ⁻² (2 Wm ⁻²)	±30 W·m ⁻² (3 Wm ⁻²)
	b) response to 5 K·h⁻¹ change is ambient temperature	±2 W·m ⁻² (0,5 Wm ⁻²)	±4 W·m ⁻² (0,5 Wm ⁻²)	±8 W·m ⁻² (1 Wm ⁻²)
	c) total zero off-set including th effects a), b) and other sources	±10 W·m ⁻² (2 W·m ⁻²)	±21 W·m ⁻² (2 W·m ⁻²)	±41 W·m ⁻² (3 W·m ⁻²)
c1	Non-stability: percentage change in responsivity per year	±0,8 % (0,25 %)	±1,5 % (0,25 %)	±3 % (0,5 %)
c2	Nonlinearity: percentage deviation from the responsivity at 500 W·m ⁻² due to the change in irradiance within 100 W·m ⁻² to 1 000 W·m ⁻²	±0,5 % (0,2 %)	±1 % (0,2 %)	±3 % (0,5 %)
c3	Directional response (for beam radiation):	±10 W·m ⁻² (4 W·m ⁻²)	±20 W·m ⁻² (5 W·m ⁻²)	±30 W·m ⁻² (7 W·m ⁻²)
	the range of errors caused by assumin that the normal incidence responsivity is valid for all directions when measur ing from any direction (with an inci- dence angle of up to 90° or even from below the sensor) a beam radiation whose normal incidence irradiance is 1 000 W·m ⁻²			

NOTE The acceptance intervals should not be used for uncertainty estimations for conditions different from the ones stated for each criterion. In particular the spectral error can be different under different conditions. The spectral error for diffuse horizontal irradiance measurements is also different from that for global horizontal irradiance.



BSRN best practices at a glance

- ~1-Hz acquisition, 1-minute stats (to catch sky variability / cloud effects)
- Ventilation (reduce IR offsets, riming, dusting)
- Shadowing LWD
- Datalogger (~0.1 W/m2)
- Store 1-Hz raw data (mV) for any review of calibration "constants"
- Store T_b , T_d of the pyrgeometer(s)
- Corrections: Cosine resp, k(Temperature), nighttime offset
- QC procedures (auto/manual)

- Instrument redundancy
- Traceability to Standards (PMOD/WRC Davos): calibration every ~2-years
 - Pyrgeom (LW): WISG
 - Pyranom (SW): WRR (group of 4 pyranometers, CM21 CM22 mainly)
 - Pyrheliom (SW direct): WSG (ACRs)
- Uncertainty (following FRM terminology is still **not completely mature**)
- This is a very active research area (see the amount of "frm4*" projects/initiatives VEG, ocean color, ...)

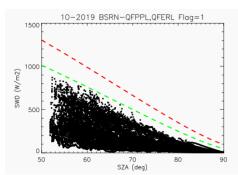
Data screening QC Tests

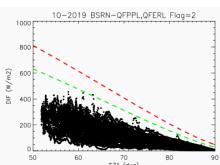


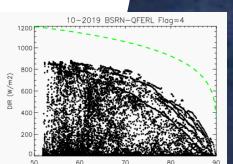
Tilting, Dusting, water on the domes, riming, Birds, Cleaning operations, Nighttime spikes, raining effects, ...

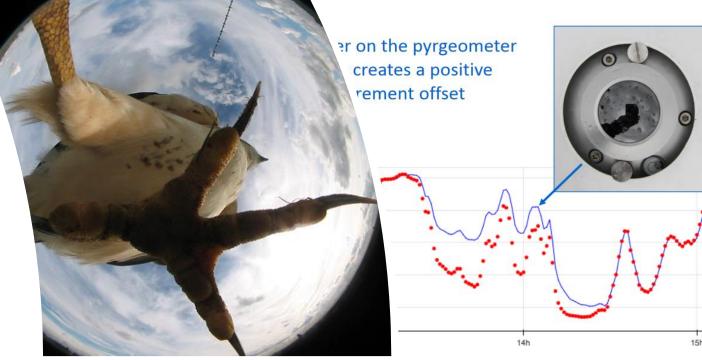


- Physically possible limits
- Extremely rare limits
- Across quantities









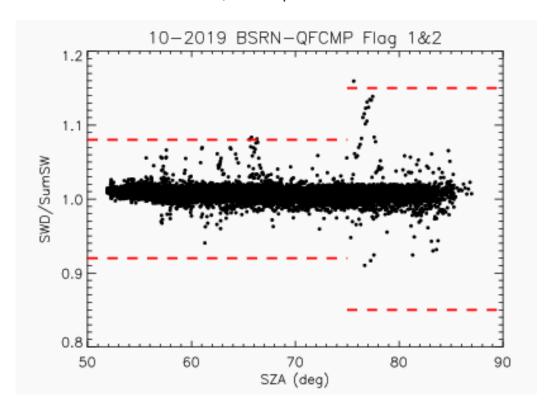


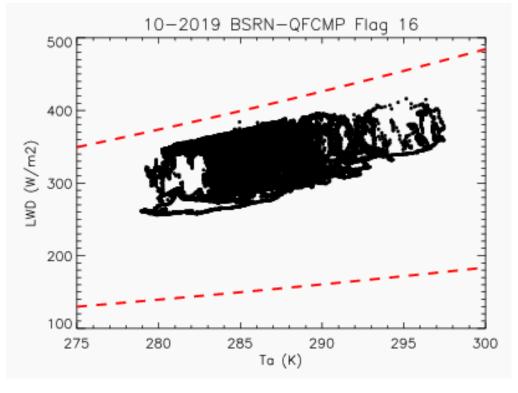
Quality Control: across quantities

Ratio of Global over Sum SW:

(Global)/(Sum SW) should be within +/- 8% of 1.0 for SZA < 75°, Sum > 50 Wm⁻² (Global)/(Sum SW) should be within +/- 15% of 1.0 for 93° > SZA > 75°, Sum > 50 Wm⁻² For Sum SW < 50 Wm⁻², test not possible

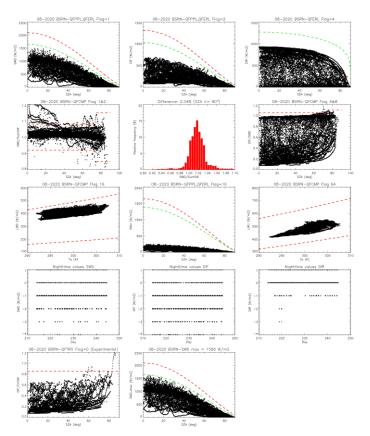
<u>LWdn to Air Temperature comparison</u> $0.4 \times \sigma T_a^4 < LWdn < \sigma T_a^4 + 25$





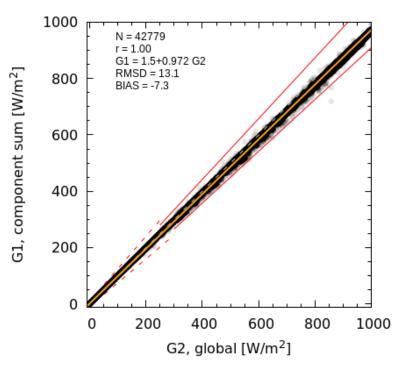


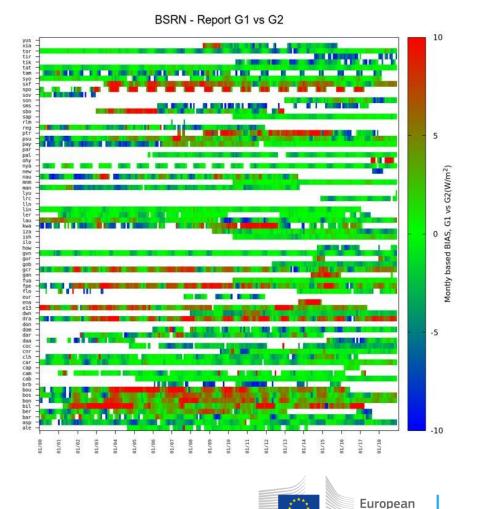
Quality Control: across quantities



Pilot: **BSRN-QC** (W. Knap, KNMI)

Global SWD G1 = dif+dirn cosZ G2 = global





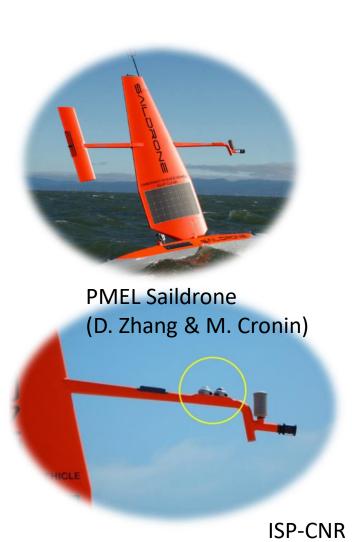
Commission

Land vs Ocean practices

	Land	Ocean	
	BSRN	vessels	buoys
Site characteristics			
Free horizon	buildings/mountains	ship structures	
Site should be representative of wider areas	point measurements	track	drifting/fixed
Accessibility	daily/weekly	continuos	monthly/yearly
Acquisitions			
Quantity measured	swd,dir,dif,lwd,(swu,lwu)		
Instruments used (technology)	thermopiles (eventually silicon for redundancy or testing)		silicon (for high freq)
Meteorological variables	T,p,RH		
Sun tracker	yes		
Acquisition rate	1hz		
Redundancy	highly recommended		
Ventilation (reduce IR offsets, riming, dusting)	all ventilated		
Shadowing LWD	yes		
Datalogger resolution	0.1 Wm-2		
Store raw data (mV), @acquisitions rate, for any review of calibration "constants"	yes		
Store pyrgeometer temperatures (Tb,Td)	yes		









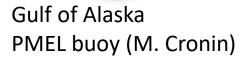
WHOI WHOTS surface mooring (R. Weller)



stabilizer

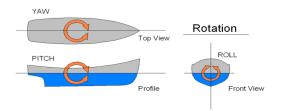
(V. Vitale)







ARM, SHIPRAD System (L. Riihimaki)



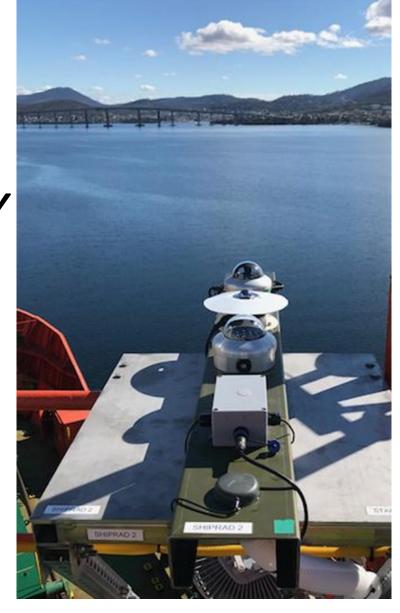




US DEPARTMENT OF ENERGY ARM SHIPRAD SYSTEM

Acknowledgements:

- Chuck Long who pioneered this system
- R. Michael Reynolds, Jim Wendell, and Emiel Hall for building it and working on calibration/characterization methodologies





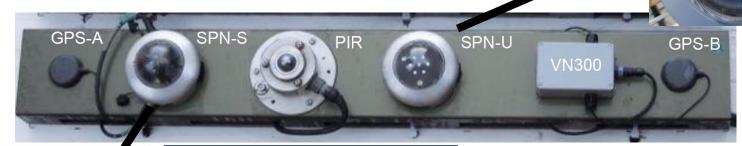
ShipRad systems correct SW irradiance for tilt and gives measurements of components:

• Diffuse SW Irradiance: Shaded SPN1 measures diffuse component of SW irradiance

Total SW Irradiance: Unshaded Delta-T SPN1

LW Irradiance: Eppley PIR

Tilt: Vector Nav 300 measures pitch, roll, heading





- --Measures components with no moving parts
- --Small thermopile sensors with fast response time
- --Internal heaters keep frost free and also mitigate IR loss

Disadvantages

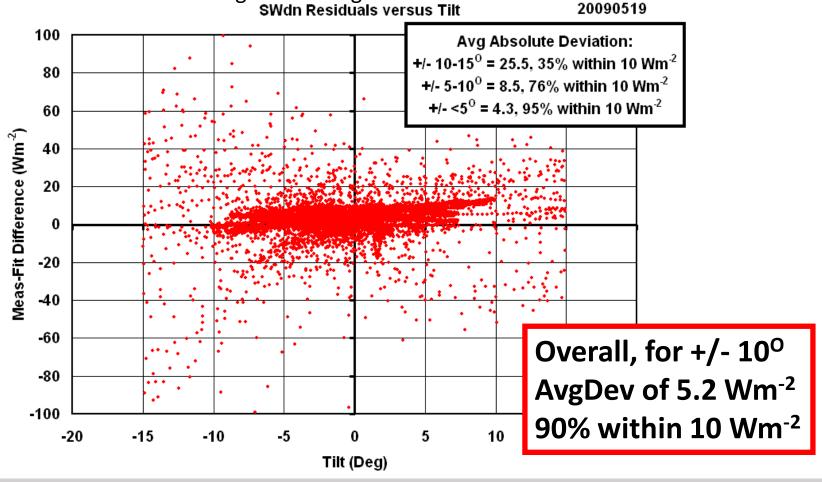
- --Differences between individual sensor leveling/cal cause step function jumps in total measurements
- --Shading pattern blocks diffuse disproportionally with zenith angle
- --Challenging to calibrate







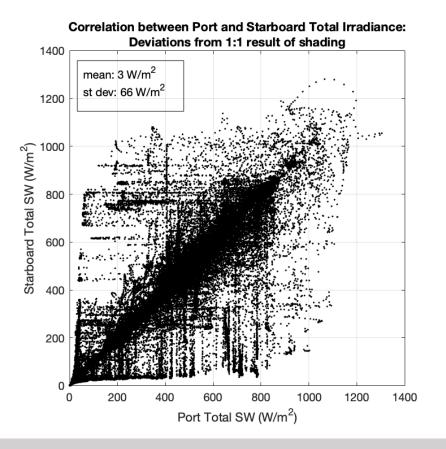
Tilt correction assumes that tilted diffuse = diffuse on a horizontal surface. This assumption is valid for small angles < 10 degrees

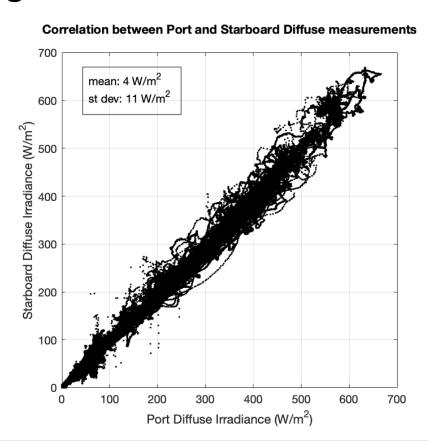






Port and Starboard Comparison—Total shows deviations due to shading not seen in diffuse

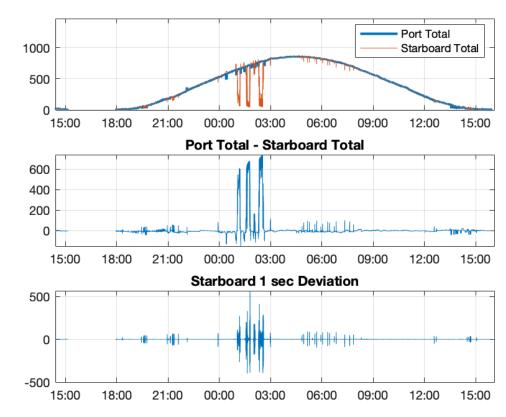






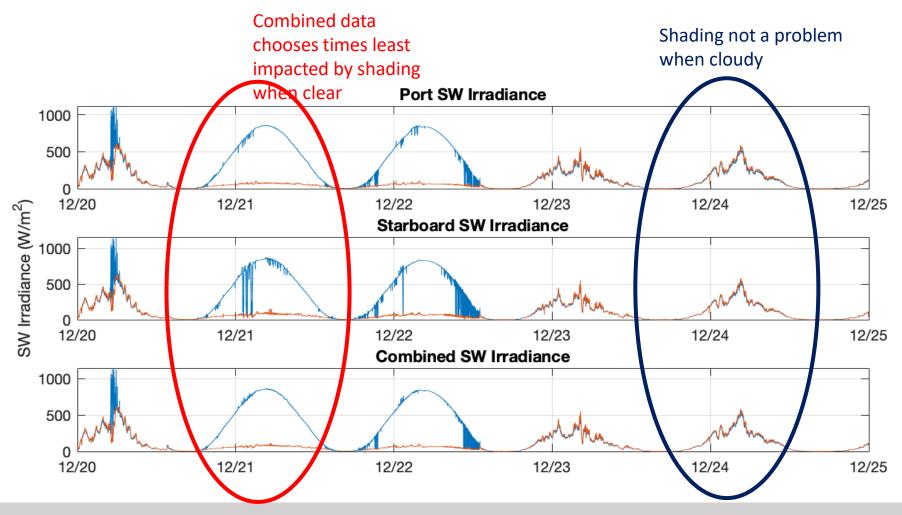
Shading correction methodology

- Downwelling LW & Diffuse SW—average of both measurements when tilt angle < 10°
- Total SW--use average unless shaded:
 - When Port/Starboard Total is >100 W/m² than Starboard/Port Total
 - Shaded when 1-second deviation greater than 5 W/m², and data from port/starboard not included





Deploying ShipRad systems on both port and starboard to reduce shading from ship structures when possible.





Towards an harmonization, and FRM concept

- Ships as a bridge between land and buoy systems
- Common field campaigns
- Active pan-tilting on land to simulate ocean waves alongside fixed platforms
- Intercomparisons of thermopiles and silicon sensors
- Sensor Throughput, thermal offsets, cosine responses

- Automatic cleaning operations
- Stabilized vs Oscillating systems
- Ocean stations on board BSRN?



References

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- https://bsrn.awi.de/other/publications/



Thank you



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EXTRA SLIDES

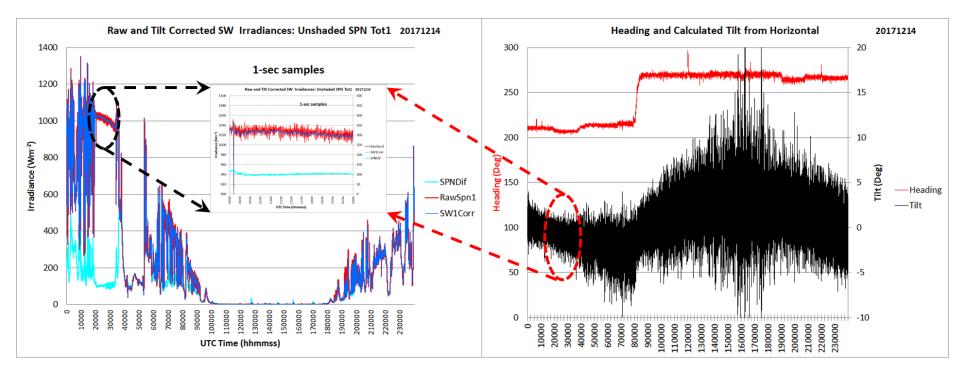


Summary of lessons of good practices for ship measurements

- SW Instrument choice important for moving platform when tracker can't be used
 - Thermopile
 - Choose model that minimizes cosine response/IR loss errors
- Calibration should be done to with traceability to the World Radiometric Reference at Davos
- Measuring components is challenging on moving platforms, but SPN1 can give measure diffuse for small tilts with no moving parts.
- In concert with more accurate SW pyranometer, SPN1 can correct tilt within 10 Wm⁻² for tilt less than 10°.



Example of tilt correction, Dec. 14, 2017



A brief nearly clear-sky period (dashed circle) shows the effectiveness of the preliminary tilt correction. As the zoom plot shows, the noise in the 1-second samples is decreased from a spread of 30-40 Wm⁻² to only a few Wm⁻². This despite the rapidly changing tilt from horizontal (black) shown in the right hand plot.

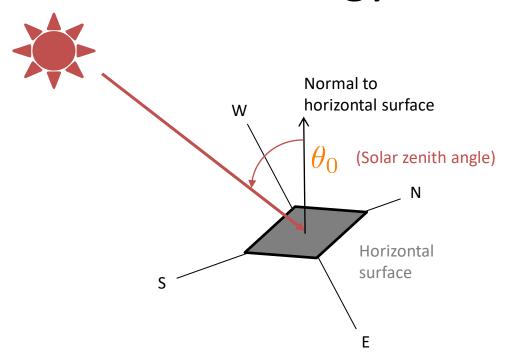


Causes of Errors in SPN1 measurements

Badosa (2014) identifies the main errors and differences in SPN1 measurements in detail. These are summarized here.

- 1. Calibration mismatch between detectors can cause jumps in the Direct part of the output as the sun moves across the sky, changing which of the detectors are fully exposed.
- 2. Lensing of light by the glass dome can cause an additional mismatch between detectors which varies with solar position.
- 3. Detector cosine response can cause a changing Direct beam sensor response which varies with solar zenith angle.
- 4. The SPN1 diffusers have a reduced transmission of blue light. This causes a variation in Diffuse sensitivity between blue-sky and cloudy conditions which is not fully corrected by the instrument.
- 5. The shape of the shadow mask pattern gives an effective opening angle which varies with solar position, between ±5° and ±20°. This changes the measured partition between Direct and Diffuse light in conditions with a large solar aureole.
- There are smaller effects due to temperature change, internal electronics, time response and soiling.





Relationship between Total SW and components on horizontal surface

$$G = D + N\mu_0$$

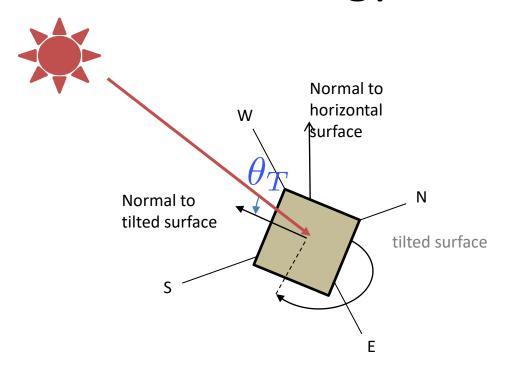
G: Total SW irradiance

D: Diffuse SW irradiance

N: Direct normal irradiance

$$\mu_0 = cos(\theta_0)$$





Relationship between Total SW and components on tilted surface

$$G_T = D_T + N\mu_T$$

 G_T : Total SW on tilted surf

 D_T : Diffuse SW on tilted surf

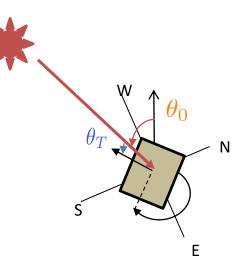
N: Direct normal irradiance

$$\mu_T = cos(\theta_T)$$



$$G = G_T \left(\frac{\mu_0 + D_N}{\mu_T + D_T} \right)$$

Equation for total irradiance as a function of measured variables



 $D_T, G_T: \;\;$ Measured by ShipRad

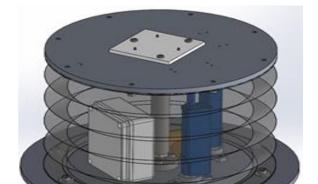
 $\mu_T = cos(heta_T)$: Calculate tilt zenith angle as a function of pitch, roll, heading

 $D=D_T: \;\;$ Assume Diffuse and tilted Diffuse equal for small tilt angles

 μ_0, N : Calculated from other measurements



Radiation measurements on a ship



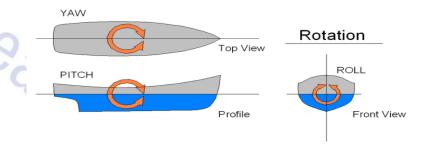
TARGET: development of a system able to mantain the

horizontal reference

APPLICATIONS: radiation measurements on a mobile platform (ship,

buoy), telemetry etc.















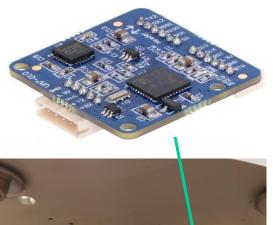
The Inertial measurement UNIT

Along each axis 3 sensors are oriented: 1 accelerometer, 1 gyroscope, 1 magnetometer. We use the signals of the first two only.

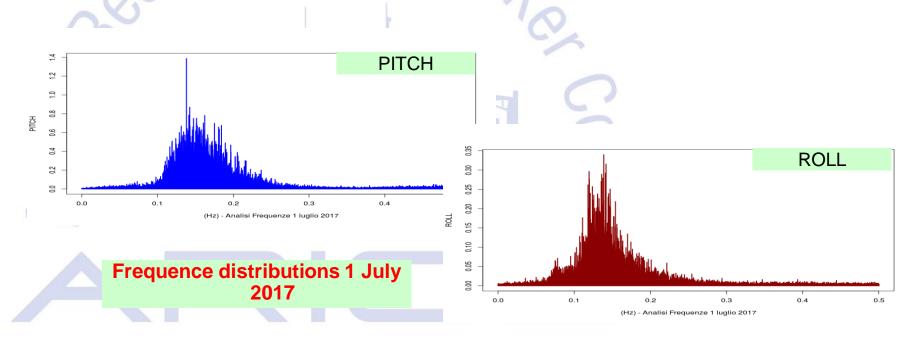
the accelerometers allow, by detecting the gravitational acceleration, to calculate the angles of roll and pitch.

The gyroscopes measure the angular velocity [degree / s], and processed able to remove acceleration component induced by translation movements on the axis.

The IMU unit is connected to the custom board CPU, and provides all the data necessary to the PID algorithm to calculate the movements along the axes (dirention and speed).









Quality Control: PPL, ERL

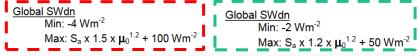
BSRN-Toolbox

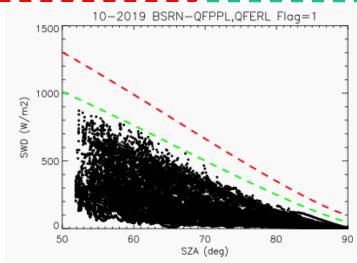
doi:10.1594/PANGAEA.901332

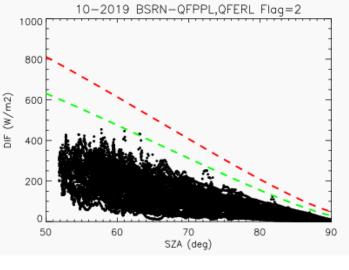
- Physically possible limits
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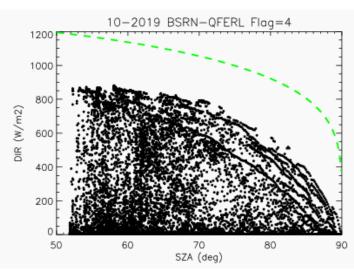
BSRN Global Network recommended QC tests, V2.0

C. N. Long and E. G. Dutton









https://bsrn.awi.de/fileadmin/user_upload/bsrn.awi.de/Publications/BSRN_recommended_QC_tests_V2.pdf

